



COMMONWEALTH of VIRGINIA

DEPARTMENT OF ENVIRONMENTAL QUALITY

Street address: 1111 E. Main Street, Suite 1400, Richmond, Virginia 23219

Mailing address: P.O. Box 1105, Richmond, Virginia 23218

www.deq.virginia.gov

Matthew J. Strickler
Secretary of Natural Resources

David K. Paylor
Director

September 27, 2018

Mr. Brian Clauto
Senior Environmental Coordinator
EQT Corporation
555 Southpointe Blvd, Suite 200
Canonsburg, PA 15317

Transmitted electronically to: BClauto@eqt.com

Re: Mountain Valley Pipeline LLC
Project Location: MVP Earth Oven (Pipeline Right-of-way Reroutes)
DEQ SWM #: MVP-18-08
Erosion and Sediment Control (ESC) and Stormwater Management (SWM) Plans

Dear Mr. Clauto:

The Department of Environmental Quality (DEQ) received combined Stormwater Management and Erosion & Sediment Control Plans for supportive ancillary areas identified as MVP Earth Oven on September 14, 2018.

The plans received Earth Oven September 14, 2018 are found to be in accordance with the *Virginia Stormwater Management Act and Regulations* and the *Virginia Erosion and Sediment Control Law and Regulations* and are approved. This approval authorizes MVP to begin land disturbing activities consistent with these plans. **No modifications, updates or additions may be made to the approved Plans without obtaining prior approval from DEQ. Additionally, approval of the ESC and SWM Plans does not relieve the owner and/or operator of complying with all other federal, state, or local laws and regulations.**

As provided by Rule 2A:2 of the Supreme Court of Virginia, you have thirty (30) days from the date you received this decision within which to appeal this decision by filing a notice of appeal in accordance with the Rules of the Supreme Court of Virginia with the Director, Virginia Department of Environmental Quality.

Mountain Valley Pipeline, LLC
DEQ SWM #: MVP-18-08
September 27, 2018
Page 2

It is the responsibility of the owner and/or operator to ensure that the project is constructed in accordance with the approved Plans and accompanying specifications. Upon completion of the project, the owner and/or operator will be required to submit construction record drawings for all permanent stormwater management facilities (i.e., post-development best management practices) constructed in accordance with the approved Plans.

Please contact Mr. Benjamin Leach at 804-698-4037 or Benjamin.leach@deq.virginia.gov if you have any questions about this letter.

Sincerely,



Jaime B. Robb, Manager
Office of Stormwater Management

Cc: Benjamin Leach, DEQ-CO
Jerome Brooks, Water Compliance Manager

Enclosure



September 14, 2018

Commonwealth of Virginia
Department of Environmental Quality
ATTN: Benjamin Leach
629 East Main Street
Richmond, Virginia 23218

Re: Spread 10 Modifications –Pipeline Re-Route from STA 13068+46 to 13117+12, Relocation of Mainline Valve No. 29 (MLV-29) Site and Access Road, and Other Changes to Associated Access Roads and Additional Temporary Work Spaces (ATWS)

Dear Mr. Leach:

Mountain Valley Pipeline, LLC (MVP) plans to re-route the pipeline alignment from STA 13068+46 to 13117+12. Additionally, MVP-MLV-29 will be relocated to be in compliance with PHMSA required mainline valve spacing, and access road MVP-FR-292.01 has been renamed as MVP-MLV-AR-29.01 and redesignated as permanent to allow permanent access to the valve site; access road MVP-MLV-AR-29 has been renamed as MVP-FR-292.01A and redesignated as temporary. Other changes include the addition of MVP-ATWS-1483 and adjustment of MVP-ATWS-1482 due to the pipeline re-route. These changes are modifications to what was proposed per the Spread 10 Erosion and Sediment Control (ESC) and Stormwater Management (SWM) Plans that were submitted and approved on March 26, 2018. Therefore, the following deliverables are being submitted to the Commonwealth of Virginia (Commonwealth), Department of Environmental Quality (DEQ) for review and approval:

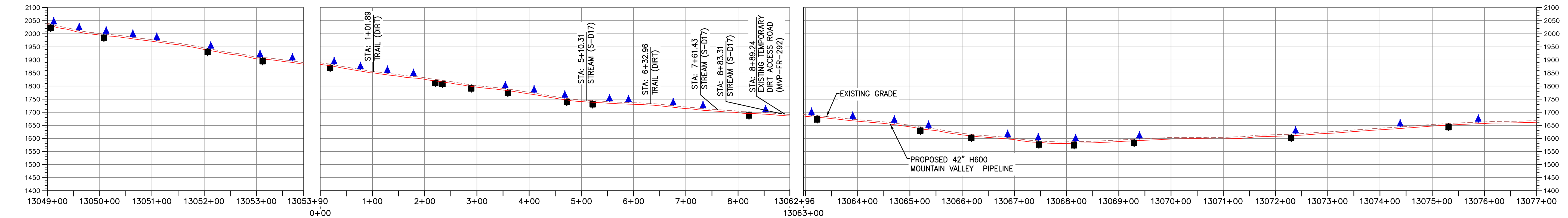
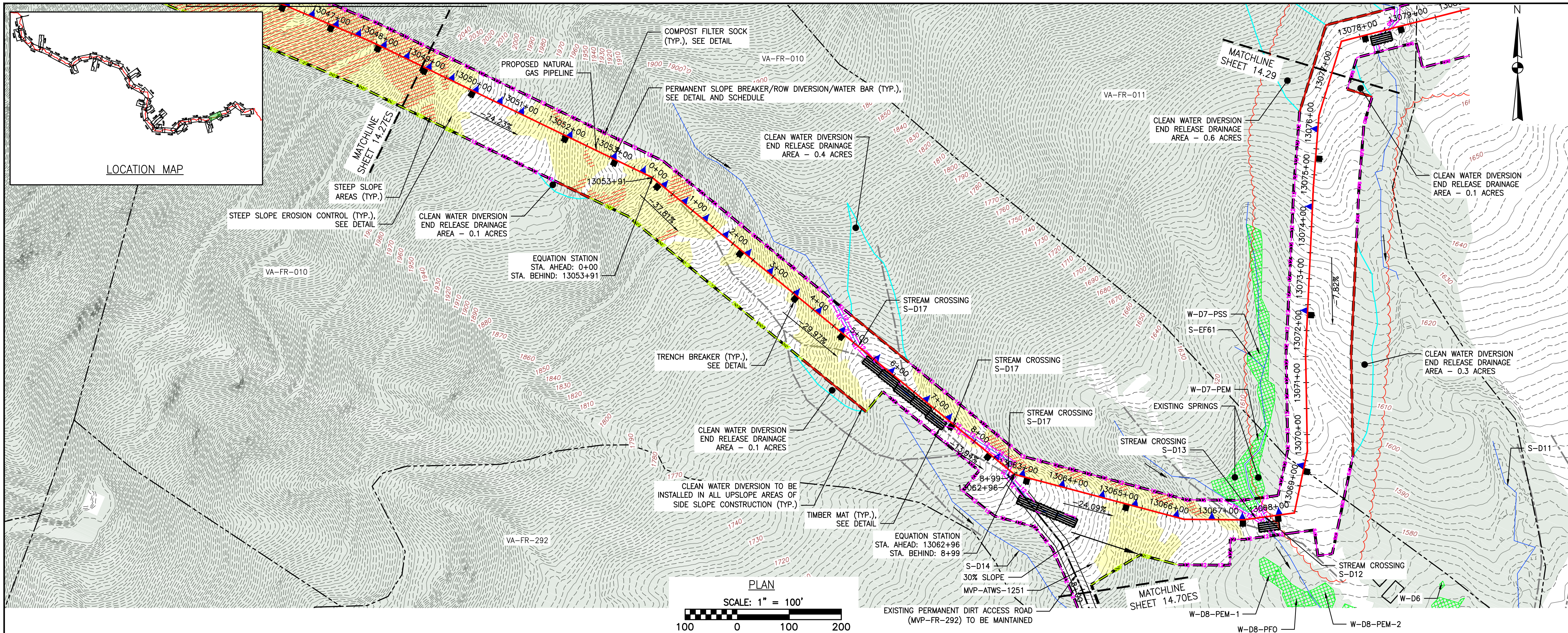
1. Spread 10 ESC Plans – Sheets No. 14.28ES, 14.29ES, and 14.30ES
2. Calculations supporting the sizing of the proposed temporary culvert shown on Sheet 14.30ES
3. Calculations supporting the sizing of the proposed riprap apron shown on Sheet 14.30ES
4. Spread 10 Clean Water Diversion Pipe Drainage Area Maps – Figure 6 of 11
5. Spread 10 PC Plans – Sheets No. 14.28PC, 14.29PC, and 14.30PC
6. Spread 10 General Details – Sheet No. 0.09
7. Spread 10 Drainage Maps (i.e., Spread 10 Water Quantity Exhibits) – Figures 26, 27, and 28 of 55
8. Spread 10 Water Quantity Calculations for New Impervious Cover
9. Spread 10 New Impervious Cover Stormwater Drainage Exhibits – Figure 007

Note that a complete list of waterbar end treatment and MLV Site coordinate locations, as well as updated Water Quality Exhibits/Calculations and ESC/SWM Narratives (if required), will be provided by spread after all modifications have been submitted and approved by the DEQ. MVP looks forward to continuing to work with the DEQ regarding this Project. Please feel free to contact me if you have questions or need any additional information.

Sincerely,

A handwritten signature in blue ink, appearing to read "B. M. Clauto".

Brian M. Clauto
Senior Environmental Coordinator
EQT Corporation
724-873-3465
bclauto@eqt.com



LEGEND

- PROPOSED LIMIT OF DISTURBANCE
- STREAM
- USDA FOREST SERVICE (NATIONAL FOREST) LANDS
- APPALACHIAN NATIONAL SCENIC TRAIL
- EXISTING ROAD/TRAIL
- EXISTING PROPERTY LINE
- EXISTING STATE LINE
- EXISTING COUNTY LINE
- POND
- WETLAND
- ACID FORMING MATERIAL
- EXISTING FOREST
- PROPOSED ACCESS ROAD CENTERLINE
- PROPOSED PIPELINE
- PROPOSED SILT FENCE (SEE NOTE 5)
- PROPOSED SUPER SILT FENCE (SEE DETAIL MVP-ES9.2)
- PROPOSED REINFORCED FILTRATION DEVICE (SEE DETAILS MVP-ES9, 9.1, 9.2, 9.3)
- ORANGE CONSTRUCTION SAFETY FENCE
- PROPOSED COMPOST FILTER SOCK (SEE DETAILS MVP-ES3, 3.1, 3.2)
- PROPOSED COMPOST FILTER SOCK (SEE DETAILS MVP-ES3, 3.1, 3.2)
- PROPOSED COMPOST FILTER SOCK (SEE DETAILS MVP-ES3, 3.1, 3.2)
- GRASS-LINED CHANNEL (SEE DETAIL MVP-ES39)
- CLEAN WATER DIVERSION PIPE
- CLEAN WATER DIVERSION DIKE (SEE DETAIL MVP-ES50 AND MVP-ES51)
- STREAM FLOW DIRECTION
- FEMA 100 YEAR FLOODPLAIN
- DRAINAGE AREA BOUNDARY
- TIMBER MAT (SEE DETAIL MVP-ES37)
- STEEP SLOPE EROSION CONTROL (SEE NOTE 2)
- STEEP SLOPE AREAS (SEE NOTE 4)
- PROPOSED ROCK CONSTRUCTION ENTRANCE
- PROPOSED TRENCH BREAKER (SEE DETAIL MVP-20)
- TEMPORARY ROW DIVERSION/WATER BAR (SEE DETAIL MVP-17)
- PERMANENT SLOPE BREAKER/ROW DIVERSION/WATER BAR (SEE DETAIL MVP-17)

NOTES:

- TOPSOIL SEGREGATION WILL BE PERFORMED IN ALL IMMEDIATE CONSTRUCTION AREAS OF THE PROJECT IN ACCORDANCE WITH DETAILS MVP-ES46.1 THROUGH MVP-ES46.3.
- FLEXITERRA, EARTHGUARD OR EQUIVALENT MAY BE USED AS A SUBSTITUTE TO EROSION CONTROL BLANKET AS DIRECTED BY MVP.
- CONTRACTOR IS RESPONSIBLE TO IDENTIFY ALL UTILITIES. THE UTILITY LINES SHOWN ON THE PLAN ARE FOR INFORMATIONAL PURPOSES ONLY AND DO NOT REPRESENT SURVEYED LINE INFORMATION.
- SLOPES OF 30' OR GREATER EXIST. CONSTRUCTION FOR STEEP SLOPES TO BE PERFORMED USING STEEP SLOPE TECHNIQUES IDENTIFIED IN THE DETAIL SHEETS. ALSO REFER TO THE SITE-SPECIFIC DESIGN OF STABILIZATION MEASURES IN SELECTED HIGH-HAZARD PORTIONS OF THE ROUTE OF THE PROPOSED MOUNTAIN VALLEY PIPELINE PROJECT.
- WHERE CONSTRUCTION CONDITIONS PRECLUDE THE USE OF DIVERSION DITCHES DUE TO SITE CONDITIONS THE CONTRACTOR WILL INSTALL SILT FENCE AT THE DIRECTION OF MVP.
- IMPROVEMENTS TO PERMANENT AND TEMPORARY ACCESS ROADS WILL BE PERFORMED PER THE SITE SPECIFIC ACCESS ROAD DETAILS.
- TEMPORARY ACCESS ROAD CROSSING OF STREAMS AND WETLANDS WILL UTILIZE TIMBERMATS. ANY PERMANENT ROAD CROSSINGS WILL BE CONDUCTED VIA CULVERTS.
- ALL NON VMRC STREAM CROSSINGS WILL BE PERFORMED AS DESCRIBED IN THE STREAM CROSSING TABLE INCLUDED IN THIS PACKAGE.

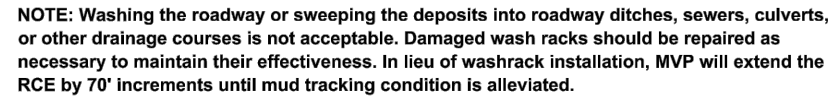
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NO.	DATE	CHKD.	APPD.	NO.	DATE	CHKD.	APPD.	NO.	DATE	CHKD.	APPD.	NO.	DATE
8	08/03/18	JJZ	RE	DW									
7	06/22/18	KAL	RE	DW									
6	03/16/18	KAL	RE	DW									
5	03/04/18	KAL	RE	DW									
4	02/27/18	KAL	RE	DW									
3	02/05/18	KAL	RE	DW									
REVISIONS:													

Mountain Valley Pipeline	
EROSION AND SEDIMENT CONTROL PLANS	
MOUNTAIN VALLEY PIPELINE PROJECT - H600 LINE	
SPREAD 10 - FRANKLIN COUNTY, VIRGINIA	
MOUNTAIN VALLEY PIPELINE, LLC	
2200 ENERGY DRIVE	
CANONSBURG, PA 15317	

TETRA TECH	
complex world CLEAR SOLUTIONS™	
661 ANDERSEN DRIVE	
FOSTER PLAZA 7	
PITTSBURGH, PA 15220	

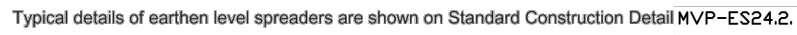
EROSION AND SEDIMENT CONTROL PLANS	
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DAVID J. WALLNER Lic. No. 0402057593 Professional Engineer	
DRAWN BY:	JJZ
CHECKED BY:	RE
APPROVED BY:	DW
DATE:	08/03/2018
SCALE:	AS SHOWN
SHT. NO. 14.28ES OF 14.81ES	REVISION



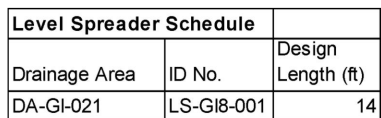
ENVIRONMENTAL DETAIL

DRAWING NO. 1412-5000



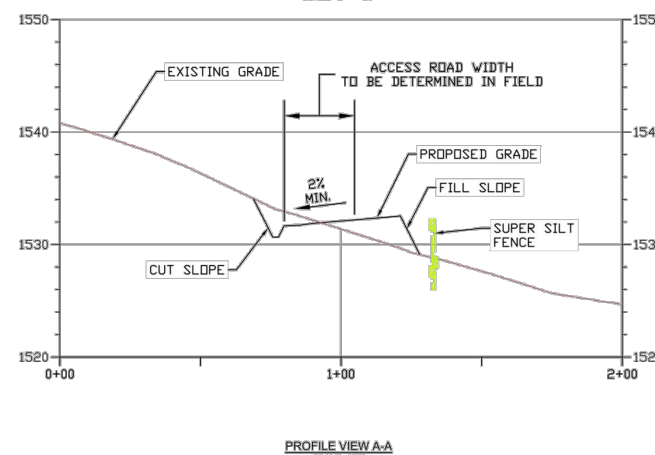
ENVIRONMENTAL DETAIL

DRAWING NO. 113-50011



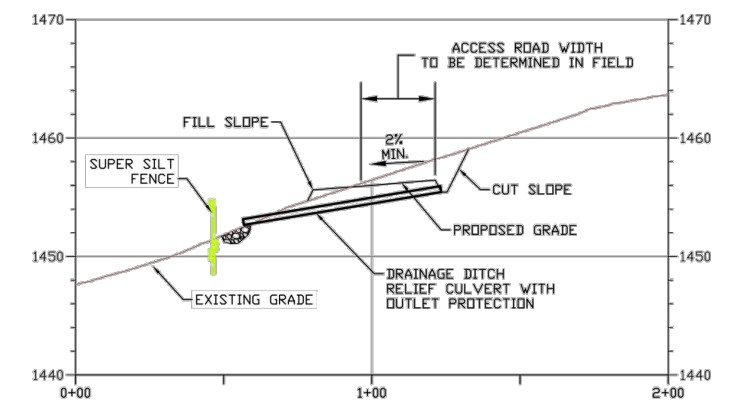
ENVIRONMENTAL DETAIL

DRAWING NO. 1415-5001-2



ENVIRONMENTAL DETAIL

DRAWING NO. 11112-5034



ENVIRONMENTAL DETAIL

RADIUS VALLEY DETAIL



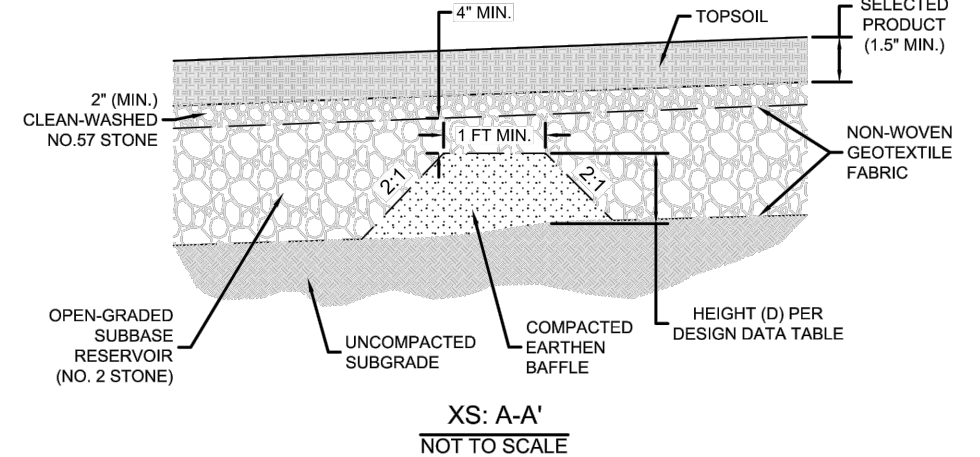
1. THICKNESS OF ASHTO #3 STONE/AGGREGATE LAYER FOR MLV PADS TO BE BETWEEN 8" AND 20" DEPENDING ON THE STORAGE VOLUME NEEDED TO MEET STORMWATER QUANTITY REQUIREMENTS.
2. THICKNESS OF ASHTO #3 STONE/AGGREGATE LAYER FOR ACCESS ROADS TO BE A MINIMUM OF 8" OR MORE AS DIRECTED.
3. COMPACT SUBGRADE PRIOR TO BACKFILL PLACEMENT. FOR BACKFILL, A MIN. 95% COMPACTION (ASTM D 690) IS REQUIRED.
4. UNSUITABLE MATERIAL SHALL BE REMOVED PRIOR TO SUBGRADE COMPACTION AND BACKFILL PLACEMENT. ADDITIONAL SUBGRADE COMPACTION NOT REQUIRED FOR MLV PADS.

ENVIRONMENTAL DETAILS

PERMANENT ACCESS F



1. INSTALLATION OF GEOGRID SHALL BEGIN AT 5-FEET FROM THE EDGE OF PUBLIC / VDOT ROADS TO ACCOMMODATE ANY CULVERTS AND TURNING OF TIRES.
2. GEOGRID SHALL NOT BE INSTALLED IN THE MAIN LINE VALVE PAD AREAS.
3. GEOGRID SHALL BE SUREGREAT PP40 OR APPROVED EQUIVALENT.



ENVIRONMENTAL DETAIL

PERMANENT ACCESS R

- ### CONSTRUCTION SEQUENCE
1. CONSTRUCTION OF THE SUBBASE ROAD Baffles SHALL BEGIN AFTER THE ENTIRE CONTRIBUTING DRAINAGE AREA HAS BEEN STABILIZED.
 2. INFILTRATION TESTS SHALL BE PERFORMED AT THE RATE OF ONE INFILTRATION TEST PER 100 LINEAL FEET OF THE 2' DEEP ACCESS ROAD, WHICHEVER IS GREATER.
 3. WHEN NECESSARY, EXCAVATORS OR BACKHOES SHOULD WORK FROM THE SIDES TO EXCAVATE THE RESERVOIR LAYER TO ITS APPROPRIATE DESIGN DEPTH AND DIMENSIONS TO ACCOMMODATE THE Baffles.
 4. NATIVE SOILS ALONG THE BOTTOM AND SIDES SHOULD BE SCARIFIED OR TILLED TO A DEPTH OF 6" TO 8" AND RESEEDED WITH GRASS SEED.
 5. INSTALL COMPACTED EARTHEN Baffles TO THE SPECIFIED DESIGN HEIGHT.
 6. THE Baffles SHALL BE CONSTRUCTED TO A MINIMUM OF 2' ABOVE THE RESERVOIR LAYER, AND THE COMPACTED EARTHEN Baffle FILL FABRIC STRIPS SHOULD OVERLAP DOWNWARDS BY A MINIMUM OF 2'-FEET AND BE SECURED A MINIMUM OF 4'-FEET BEYOND THE Baffle TO THE SUBBASE.
 7. THE Baffles SHALL BE CONSTRUCTED TO A MINIMUM OF 2'-FEET ABOVE THE RESERVOIR LAYER. EACH Baffle SHALL BE 2'-FEET-AND 4" WIDE.
 8. MAINTAIN 4-INCH MINIMUM TOP OF SUBBASE RESERVOIR.
 9. INSTALL FILL FABRIC ON TOP OF SUBBASE RESERVOIR.
 10. INSTALL 2-INCH EARTHEN Baffle CHOICE.
 11. PLACE GEOTEXTILE AND FILL WITH GRAVEL AND TOPSOIL PER GRAVEL WIDTHS AND CENTER LINE WIDTHS.
 12. SEED CENTER AREA WITH MEADOW SEED MIX PER MPMV-1S12 OR MPMV-1S13.

CONSTRUCTION INSPECTION

1. DURING MAIN LINE VALVE ANNUAL MAINTENANCE ACTIVITIES, PERFORM A VISUAL INSPECTION OF THE ACCESS ROAD TO IDENTIFY EROSION ISSUES, SEDIMENT DEPOSITION, ORGANIC DEBRIS AND STAINING OR PONDING THAT MAY INDICATE CLOGGING.
2. GRADED CENTER AISLE SHALL BE MOVED AT THE SAME INTERVAL AS MAIN LINE VALVE MAINTENANCE ACTIVITIES.
3. GRADED CENTER AISLE WILL NOT BE CONSIDERED ESTABLISHED UNTIL A GROUND COVER IS ACHIEVED THAT IS UNIFORM AND MATURE ENOUGH TO SURVIVE AND INHIBIT EROSION.

ENVIRONMENTAL DETAIL

PERMANENT ACCESS R

For 12-in pipe:

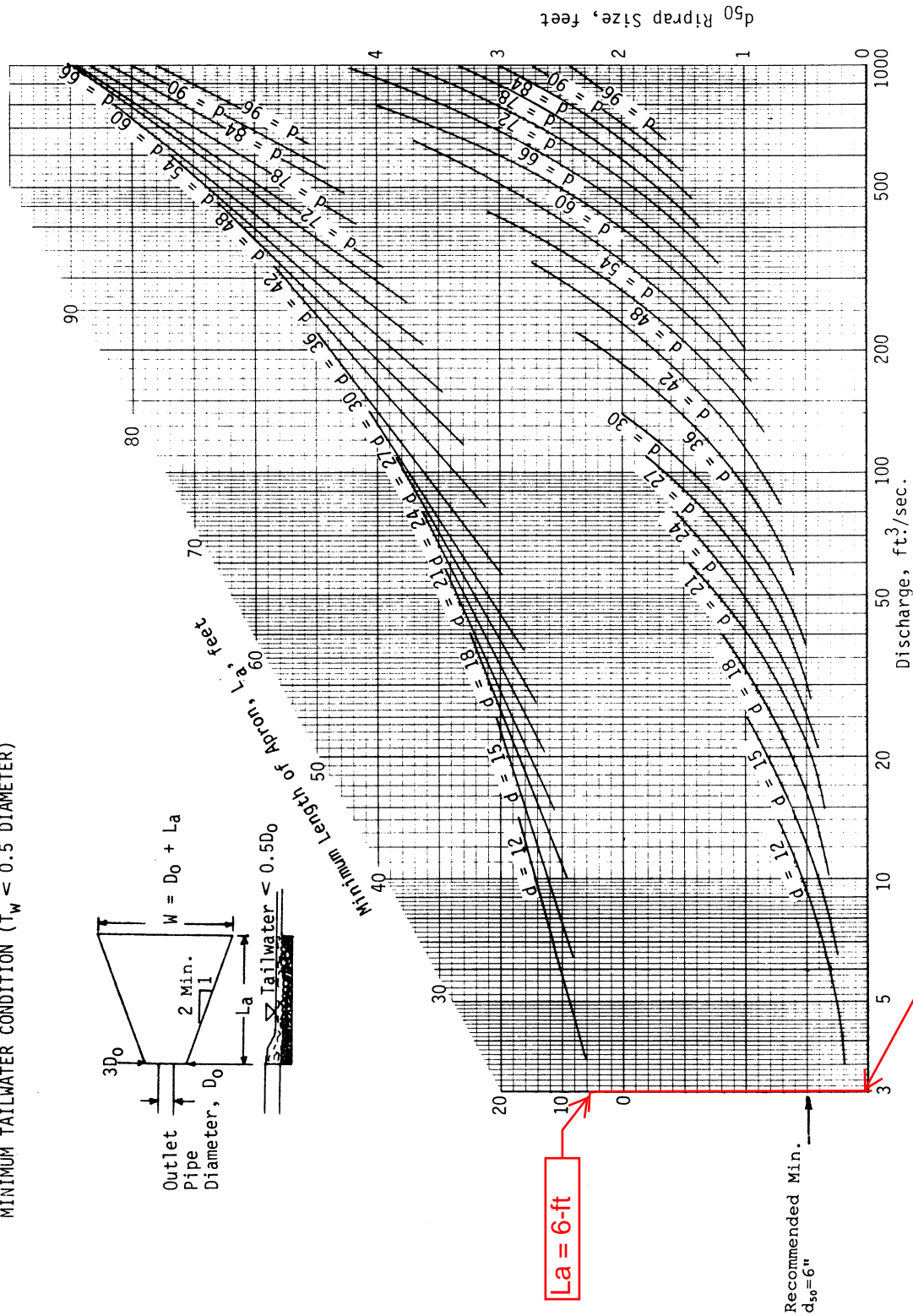
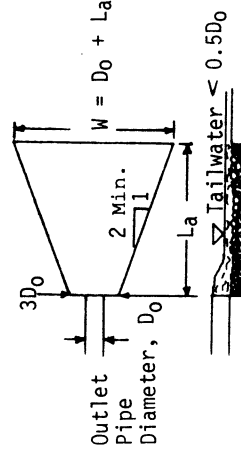
$3D_0 = 3\text{-ft}$

$La = 6\text{-ft}$

$W = 1\text{-ft} + 6\text{-ft} = 7\text{-ft}$

Riprap $d_{50} = 6\text{-in}$ (recommended minimum), so just specify **VDOT Class A1** which has a $d_{50} = 0.8\text{-ft}$ and a placement thickness (d) of 20-in.

DESIGN OF OUTLET PROTECTION FROM A ROUND PIPE FLOWING FULL
MINIMUM TAILWATER CONDITION ($T_w < 0.5$ DIAMETER)



10-Year Peak Flow Calculator

Enter Site Specific Data	T _c =	5	assumed time of concentration, min
	A =	1.5	clean water diversion drainage area, ac
	S =	0.5	weir discharge overland slope, ft/ft
Computed	i =	6.6	computed from IDF, in/hr
Enter Flow Parameters	C =	0.19	Composite runoff coefficient assuming 50% "Woods" and 50% "Pasture" land use conditions in HSG B soils with 6%+ slopes from VA SWM Handbook Volume II, Table 4-5b to be conservative
Computed 10-Year Peak Flow -----> 1.83 cfs			

Runoff	
A	Q=CiA
0.03	0.04
0.04	0.05
0.05	0.06
0.06	0.07
0.07	0.09
0.08	0.10
0.09	0.11
0.10	0.12
0.11	0.13
0.12	0.15
0.13	0.16
0.14	0.17
0.15	0.18
0.16	0.20
0.17	0.21
0.18	0.22
0.19	0.23
0.20	0.24
0.21	0.26
0.22	0.27
0.23	0.28

	Pittsylvania
Tc	i2
1	6.8
2	6.4
3	6.0
4	5.6
5	5.3
6	5.1
7	4.8
8	4.6
9	4.4
10	4.2
11	4.1
12	3.9
13	3.8
14	3.7
15	3.5
16	3.4
17	3.3
18	3.2
19	3.1
20	3.1
21	3.0
22	2.9
23	2.8
24	2.8
25	2.7
26	2.6
27	2.6
28	2.5
29	2.5
30	2.4

Temporary Culvert Pipe Sizing

Equations Used:

$$^1Q = CiA$$

$$^2\theta = 2\arccos[(r-h)/r]$$

$$^3K = [r^2*(\theta - \sin\theta)]/2$$

$$^4s = r*\theta$$

$$^5R = K/s$$

$$^6Q_{\text{pipe}} = (1.49/n)(A)(R^{2/3})(S^{1/2})$$

¹ Rational Equation for peak flow (Q)

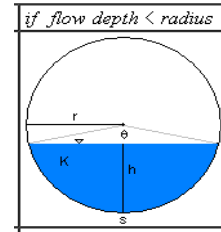
² Central angle as shown on figure

³ Flow area as shown on figure

⁴ Wetted perimeter, or arc length, as shown on figure

⁵ Hydraulic Radius

⁶ Manning Equation

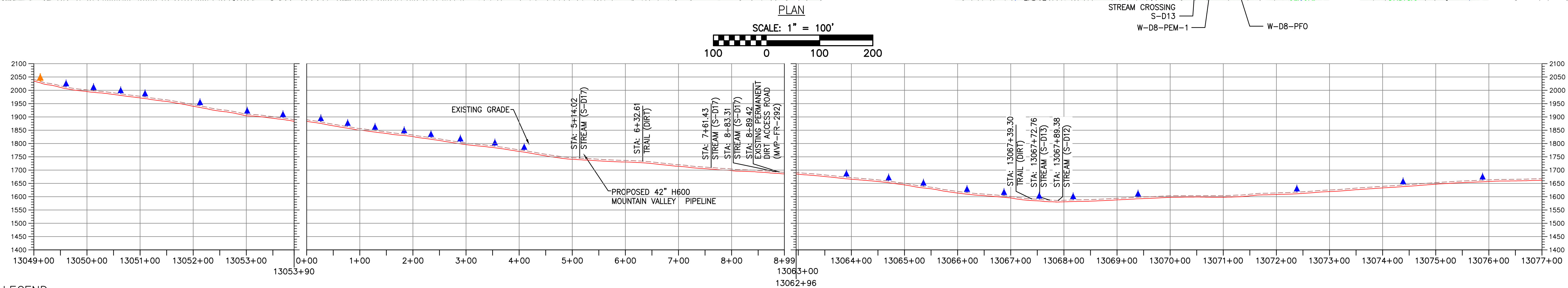
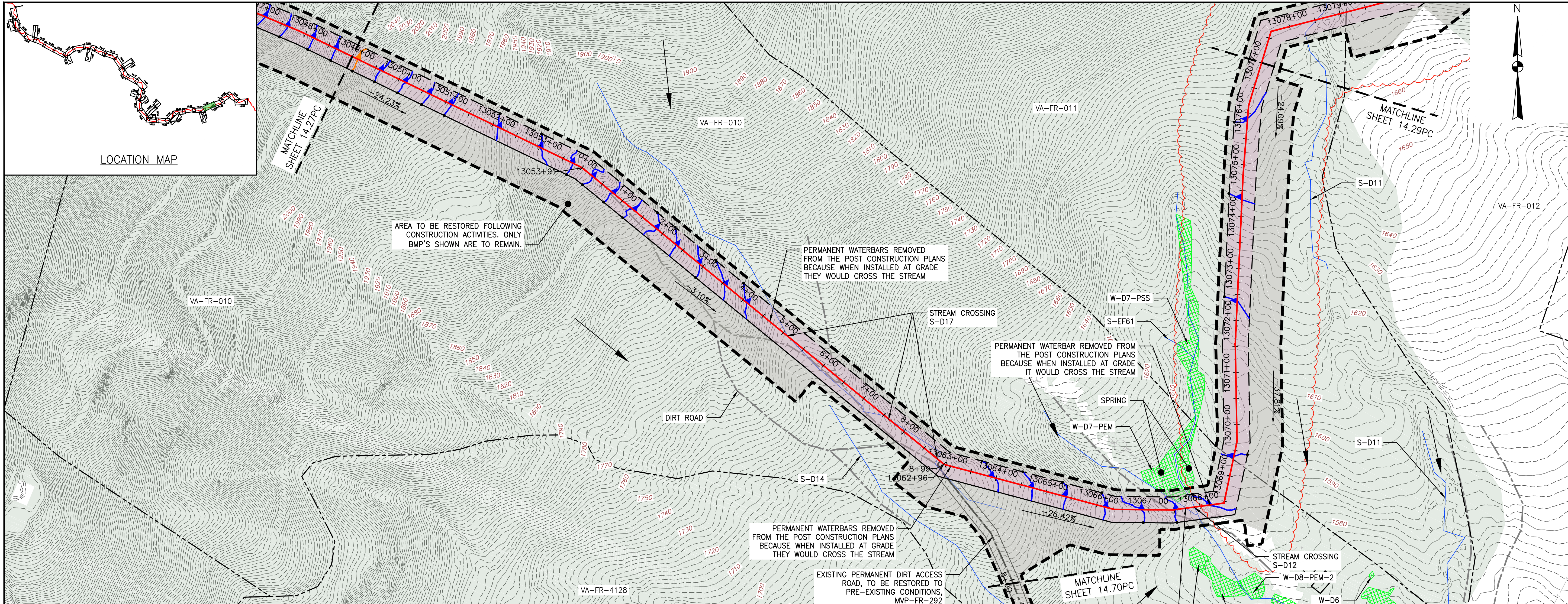


Inputs:

Inputs for Equation 1 (10-Year Peak Flow Calculations)	Runoff Coefficient, C =	0.19	Composite runoff coefficient assuming 50% "Woods" and 50% "Pasture" land use conditions in HSG B soils with 6%+ slopes from VA SWM Handbook Volume II, Table 4-5b to be conservative
	10-Year Rainfall Intensity, I (in/hr) =	6.61	Used I-D-F Curve for Pittsylvania County, assuming a 5-minute time of concentration
	Contributing Drainage Area, A (acres) =	1.5	CWD drainage area as shown on ESC Plan
Inputs for Equation 5 (Pipe Capacity Calculations)	Manning's Roughness Coefficient, n =	0.0120	Assume n=0.0120 for smooth HDPE
	Pipe Radius, r (ft) =	0.50	For 12-in pipe, the pipe radius is 6-in (or 0.5-ft)
	Flow Depth, h (ft) =	0.43	Assume that pipe capacity is limited to 40% of pipe-full-flow capacity to be conservative
	Central Angle, θ (radians) =	2.86	Assume that pipe capacity is limited to 40% of pipe-full-flow capacity to be conservative
	<u>12-in Pipe</u> Flow Area, K (sf) =	0.32	Assume that pipe capacity is limited to 40% of pipe-full-flow capacity to be conservative
	<u>12-in Pipe</u> Wetted Perimeter, s (ft) =	1.43	Assume that pipe capacity is limited to 40% of pipe-full-flow capacity to be conservative
	<u>12-in Pipe</u> Hydraulic Radius, R (ft) =	0.23	Assume that pipe capacity is limited to 40% of pipe-full-flow capacity to be conservative

Calculations:

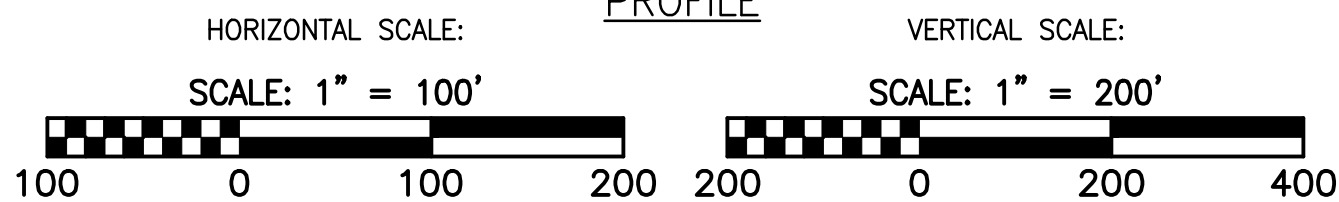
Equation 1 Results (10-Year Peak Flow Calculations)	10-Year Peak Flow, Q (cfs) =	1.83	Temporary culvert must be sized to safely convey the 10-year 24-hour minimum flood frequency per Chapter 8 of the VDOT Drainage Manual since it is a small road with minimal traffic flow
Equation 5 Results (Pipe Capacity Calculations)	<u>12-in Pipe, 1.5% Slope</u> Flow Capacity, Q _{pipe} (cfs) =	1.82	In order to safely convey the 10-year peak flow, the culvert must have a minimum slope of approx. 1.5%. Therefore, the pipe as shown on the ESC Plan would have to have a fall of at least 0.45-ft over its length (approx. 30-ft)
	<u>12-in Pipe, 2.0% Slope</u> Flow Capacity, Q _{pipe} (cfs) =	2.10	
	<u>12-in Pipe, 2.5% Slope</u> Flow Capacity, Q _{pipe} (cfs) =	2.35	
	<u>12-in Pipe, 3.0% Slope</u> Flow Capacity, Q _{pipe} (cfs) =	2.58	



LEGEND

- EXISTING CULVERT
- STREAM
- EXISTING PROPERTY LINE
- EXISTING STATE LINE
- EXISTING COUNTY LINE
- EXISTING ROAD/TRAIL
- USDA FOREST SERVICE (NATIONAL FOREST) LANDS
- ANST APPALACHIAN NATIONAL SCENIC TRAIL
- AFM ACID FORMING MATERIAL
- GRASS-LINED CHANNEL (SEE DETAIL MVP-ES39)
- PROPOSED LIMIT OF DISTURBANCE
- PROPOSED PERMANENT RIGHT OF WAY
- PROPOSED LEVEL SPREADER DIVERSION
- PROPOSED LEVEL SPREADER
- PROPOSED ACCESS ROAD CENTERLINE
- PROPOSED PIPELINE
- SURFACE WATER FLOW DIRECTION
- POND
- WETLAND
- PROPOSED CULVERT WITH OUTLET PROTECTION (SEE DETAILS MVP-ES7, 7.1)
- APPROXIMATE LOCATION OF WATER BAR END TREATMENTS (PENDING FIELD CONDITIONS)
- STREAM FLOW DIRECTION
- FEMA 100 YEAR FLOODPLAIN
- PERMANENT WATER BAR 10' END TREATMENT
- PERMANENT WATER BAR 15' END TREATMENT
- PERMANENT WATER BAR 20' END TREATMENT

PROFILE



- STEEP SLOPE AREA
- EXISTING FOREST
- PERMANENT EASEMENT RESTORED TO MEADOW CONDITION
- TEMPORARY EASEMENT RESTORED TO BRUSH CONDITION

NOTES:

- NOTE THAT ALL WATER BARS REGARDLESS OF SPECIFIED CALCULATION LENGTH ARE TO BE INSTALLED WITH 20-FT END TREATMENT LENGTHS, EXCEPT AS NOTED IN NOTE 2 BELOW.
- IN AREAS OF RIDGETOP AS NOTED IN THE TABLE ON THE KEY PLAN OF THIS PLAN SET, WATER BARS WITH END TREATMENT LENGTHS OF 10-FT WILL BE PLACED ON EITHER END.

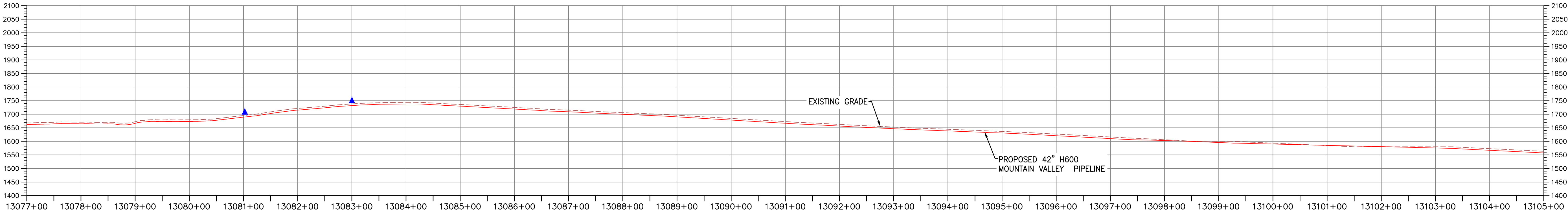
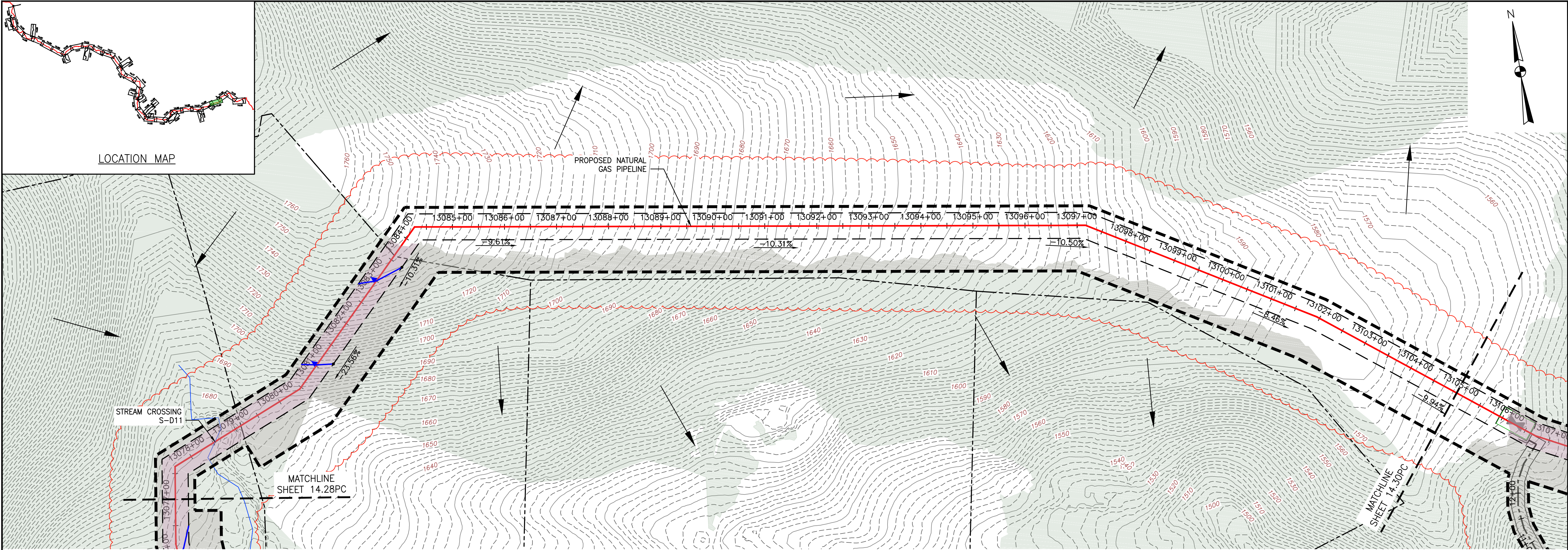
FIELD MODIFICATION		ADDRESS VADEQ COMMENTS	
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6	03/21/18	KAL	RE
5	03/16/18	KAL	RE
4	03/04/18	KAL	RE
3	02/22/18	KAL	RE
2	11/21/17	KAL	RE
NO:	DATE:	DWN:	CHKD:
APPD:			
REVISIONS:			

POST CONSTRUCTION (STORMWATER & RESTORATION) PLANS	
MOUNTAIN VALLEY PIPELINE PROJECT - H600 LINE	
SPREAD 10 - FRANKLIN COUNTY, VIRGINIA	
MOUNTAIN VALLEY PIPELINE, LLC	
555 SOUTHPOINTE BOULEVARD, SUITE 200	
CANONSBURG, PA 15317	

TETRA TECH	
complex world CLEAR SOLUTIONS™	
661 ANDERSEN DRIVE	
FOSTER PLAZA 7	
PITTSBURGH, PA 15220	

POST CONSTRUCTION (STORMWATER & RESTORATION) PLANS	
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COMMONWEALTH OF PENNSYLVANIA	
DAVID J. WALLNER	
Lic. No. 0402057593	
PROFESSIONAL ENGINEER	
DRAWN BY: KAL	
CHECKED BY: HT	
APPROVED BY: RE	
DATE: 06/22/2018	
SCALE: AS SHOWN	
SHT. NO. 14.28PC OF 14.77PC	



LEGEND

- EXISTING CULVERT
- STREAM
- - - EXISTING PROPERTY LINE
- - - EXISTING STATE LINE
- - - EXISTING COUNTY LINE
- - - EXISTING ROAD/TRAIL
- USDA FOREST SERVICE (NATIONAL FOREST) LANDS
- APPALACHIAN NATIONAL SCENIC TRAIL
- ACID FORMING MATERIAL
- GRASS-LINED CHANNEL (SEE DETAIL MVP-ES39)
- PROPOSED LIMIT OF DISTURBANCE
- PROPOSED PERMANENT RIGHT OF WAY
- >>>> PROPOSED LEVEL SPREADER DIVERSION
- ++++ PROPOSED LEVEL SPREADER
- PROPOSED ACCESS ROAD CENTERLINE
- PROPOSED PIPELINE
- SURFACE WATER FLOW DIRECTION
- POND
- WETLAND
- PROPOSED CULVERT WITH OUTLET PROTECTION (SEE DETAILS MVP-ES7, 7.1)
- APPROXIMATE LOCATION OF WATER BAR END TREATMENTS (PENDING FIELD CONDITIONS)
- STREAM FLOW DIRECTION
- FEMA 100 YEAR FLOODPLAIN
- PERMANENT WATER BAR 10' END TREATMENT
- PERMANENT WATER BAR 15' END TREATMENT
- PERMANENT WATER BAR 20' END TREATMENT
- STEEP SLOPE AREA
- EXISTING FOREST
- PERMANENT EASEMENT RESTORED TO MEADOW CONDITION
- TEMPORARY EASEMENT RESTORED TO BRUSH CONDITION

NOTES:

1. NOTE THAT ALL WATER BARS REGARDLESS OF SPECIFIED CALCULATION LENGTH ARE TO BE INSTALLED WITH 20-FT END TREATMENT LENGTHS, EXCEPT AS NOTED IN NOTE 2 BELOW.
2. IN AREAS OF RIDGETOP AS NOTED IN THE TABLE ON THE KEY PLAN OF THIS PLAN SET, WATER BARS WITH END TREATMENT LENGTHS OF 10-FT WILL BE PLACED ON EITHER END.

TETRA TECH CAD FILE PATH: X:\CADD\Pittsburgh\DOT\7157 - MVP\15 - Franklin\PC\PC VERSION 5.0.0\SPREAD 10\7157PC14.29(S10).dwg - PLOTTED ON: 9/11/2018 3:58 PM - PLOTTED BY: Rickabough, Greg - PLOT FILE: ENVIRONMENTAL_COLOR.ctb

FIELD MODIFICATION	RE	DW	DATE	DESCRIPTION
ADDRESS VADEQ COMMENTS	RE	DW		
ADDRESS VADEQ COMMENTS	RE	DW		
ADDRESS VADEQ COMMENTS	RE	DW		
RESUBMISSION USING APPROVED STORMWATER METHODOLOGY	RE	DW		
ADDRESS VADEQ COMMENTS	RE	DW		
NO.	DATE	DW	CHKD.	APPD.

POST CONSTRUCTION (STORMWATER & RESTORATION) PLANS	REVISIONS:
MOUNTAIN VALLEY PIPELINE PROJECT - H600 LINE	
SPREAD 10 - FRANKLIN COUNTY, VIRGINIA	
MOUNTAIN VALLEY PIPELINE, LLC	
2200 ENERGY DRIVE	
CANONSBURG, PA 15317	

TETRA TECH

complex world | CLEAR SOLUTIONS™

661 ANDERSEN DRIVE
FOSTER PLAZA 7
PITTSBURGH, PA 15220

POST CONSTRUCTION
(STORMWATER &
RESTORATION) PLANS

COMMONWEALTH OF PENNSYLVANIA

DAVID J. WALLNER
Lic. No. 0402057593

DRAWN BY: KAL

CHECKED BY: HT

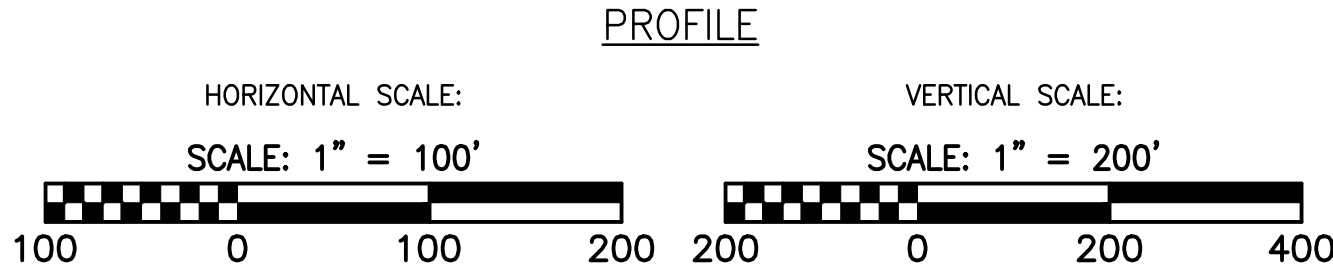
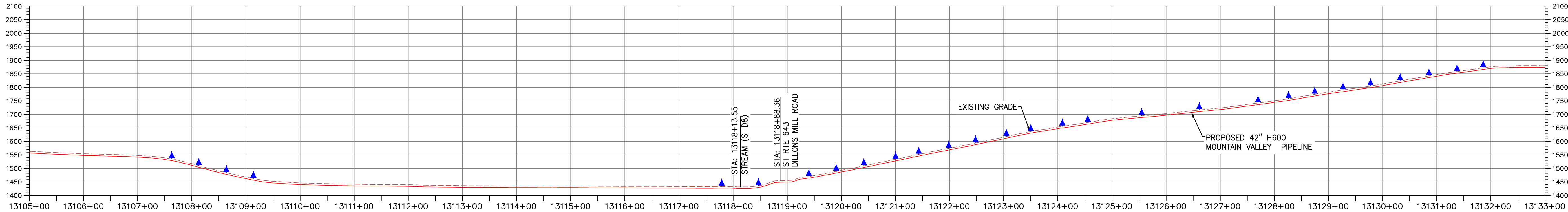
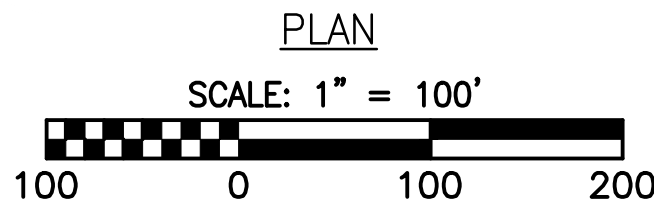
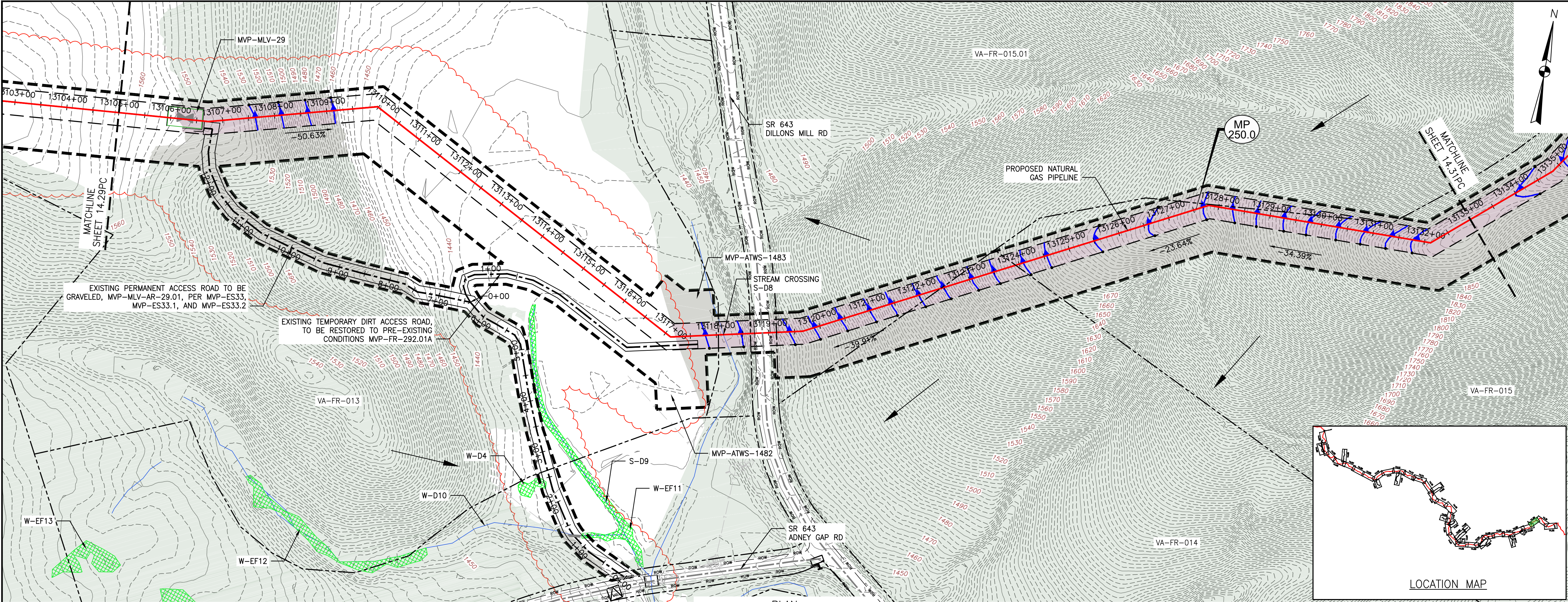
APPROVED BY: RE

DATE: 06/22/2018

SCALE: AS SHOWN

SHT. NO. 14.29PC OF 14.77PC

REVISION



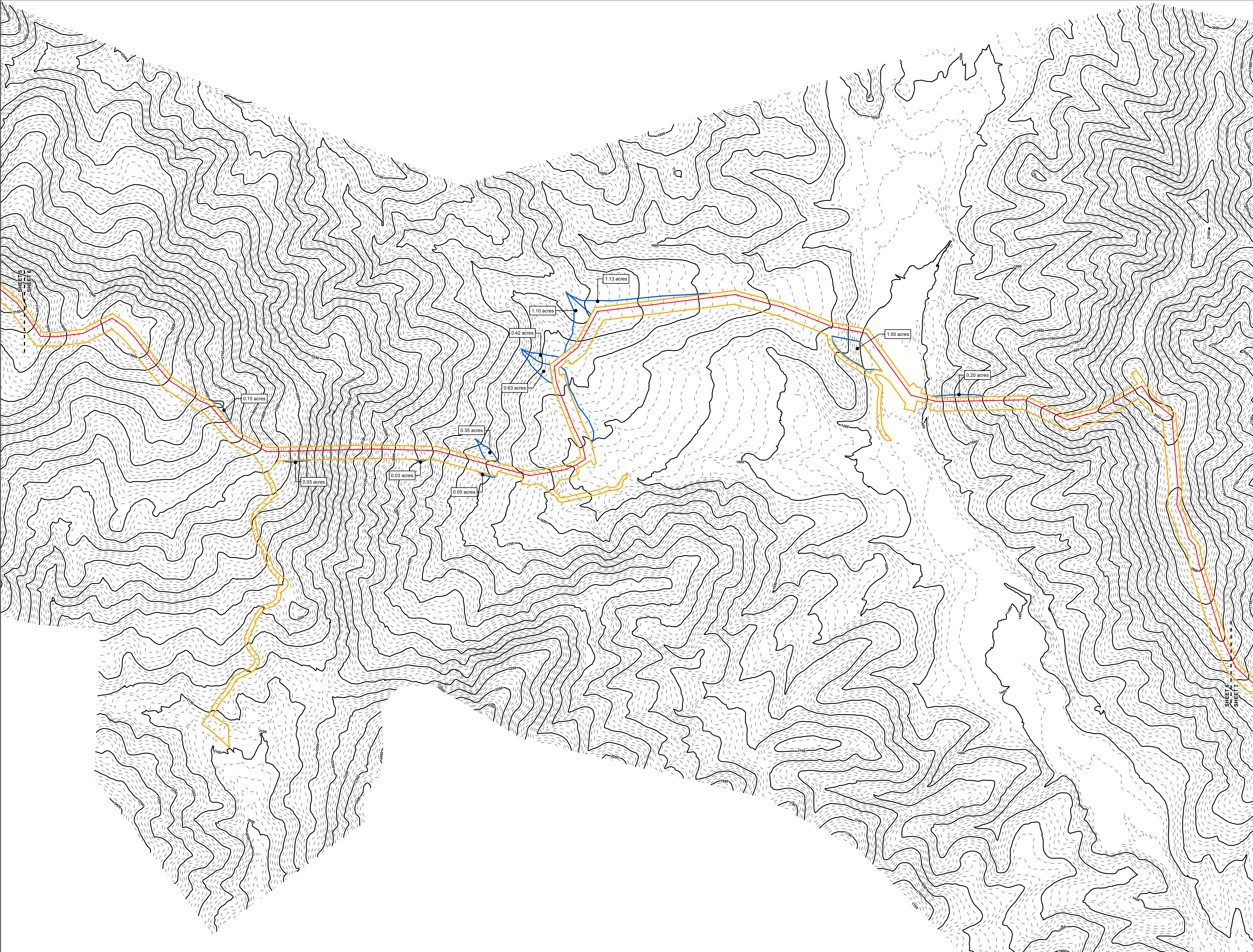
LEGEND

- | | | |
|---|---|---|
| — EXISTING CULVERT | — PROPOSED LEVEL SPREADER DIVERSION | — STREAM FLOW DIRECTION |
| — STREAM | ++++ PROPOSED LEVEL SPREADER | — FEMA 100 YEAR FLOODPLAIN |
| - - - EXISTING PROPERTY LINE | - - - PROPOSED ACCESS ROAD CENTERLINE | ▲ PERMANENT WATER BAR 10' END TREATMENT |
| - - - EXISTING STATE LINE | — PROPOSED PIPELINE | ▲ PERMANENT WATER BAR 15' END TREATMENT |
| - - - EXISTING COUNTY LINE | — SURFACE WATER FLOW DIRECTION | ▲ PERMANENT WATER BAR 20' END TREATMENT |
| - - - EXISTING ROAD/TRAIL | — POND | |
| — USDA FOREST SERVICE (NATIONAL FOREST) LANDS | — WETLAND | |
| — APPALACHIAN NATIONAL SCENIC TRAIL | — PROPOSED CULVERT WITH OUTLET PROTECTION (SEE DETAILS MVP-ES7, 7.1) | |
| — ACID FORMING MATERIAL | • APPROXIMATE LOCATION OF WATER BAR END TREATMENTS (PENDING FIELD CONDITIONS) | |
| — GRASS-LINED CHANNEL (SEE DETAIL MVP-ES39) | | |
| - - - PROPOSED LIMIT OF DISTURBANCE | | |
| - - - PROPOSED PERMANENT RIGHT OF WAY | | |

NOTES:

- NOTE THAT ALL WATER BARS REGARDLESS OF SPECIFIED CALCULATION LENGTH ARE TO BE INSTALLED WITH 20-FT END TREATMENT LENGTHS, EXCEPT AS NOTED IN NOTE 2 BELOW.
- IN AREAS OF RIDGETOP AS NOTED IN THE TABLE ON THE KEY PLAN OF THIS PLAN SET, WATER BARS WITH END TREATMENT LENGTHS OF 10-FT WILL BE PLACED ON EITHER END.

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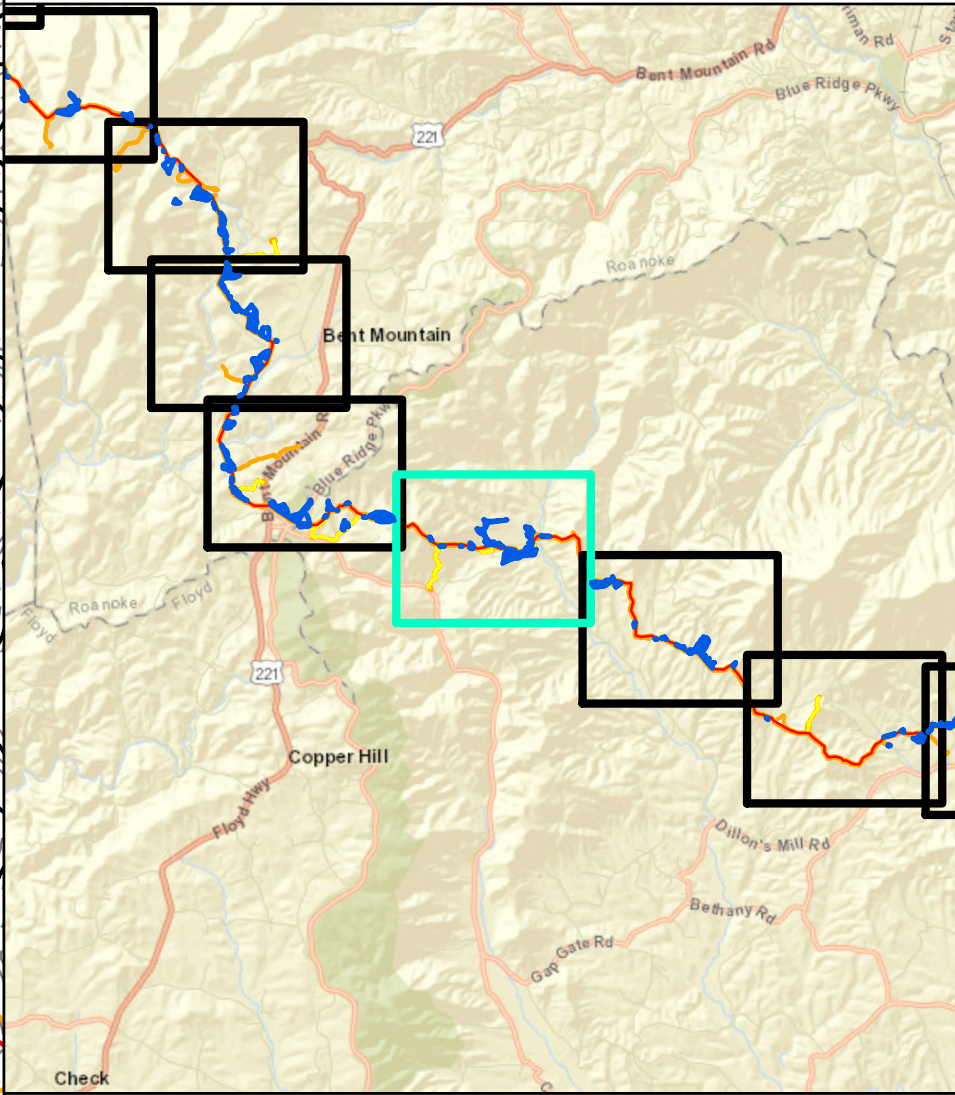
Legend

- Limit of Disturbance
- Alignment Centerline
- Permanent Access Road
- Existing 50' Contours
- Existing 10' Contours
- Drainage Area

NAD 1983 UTM 17N

1:4,800

400 0 400 800 1,200 Feet



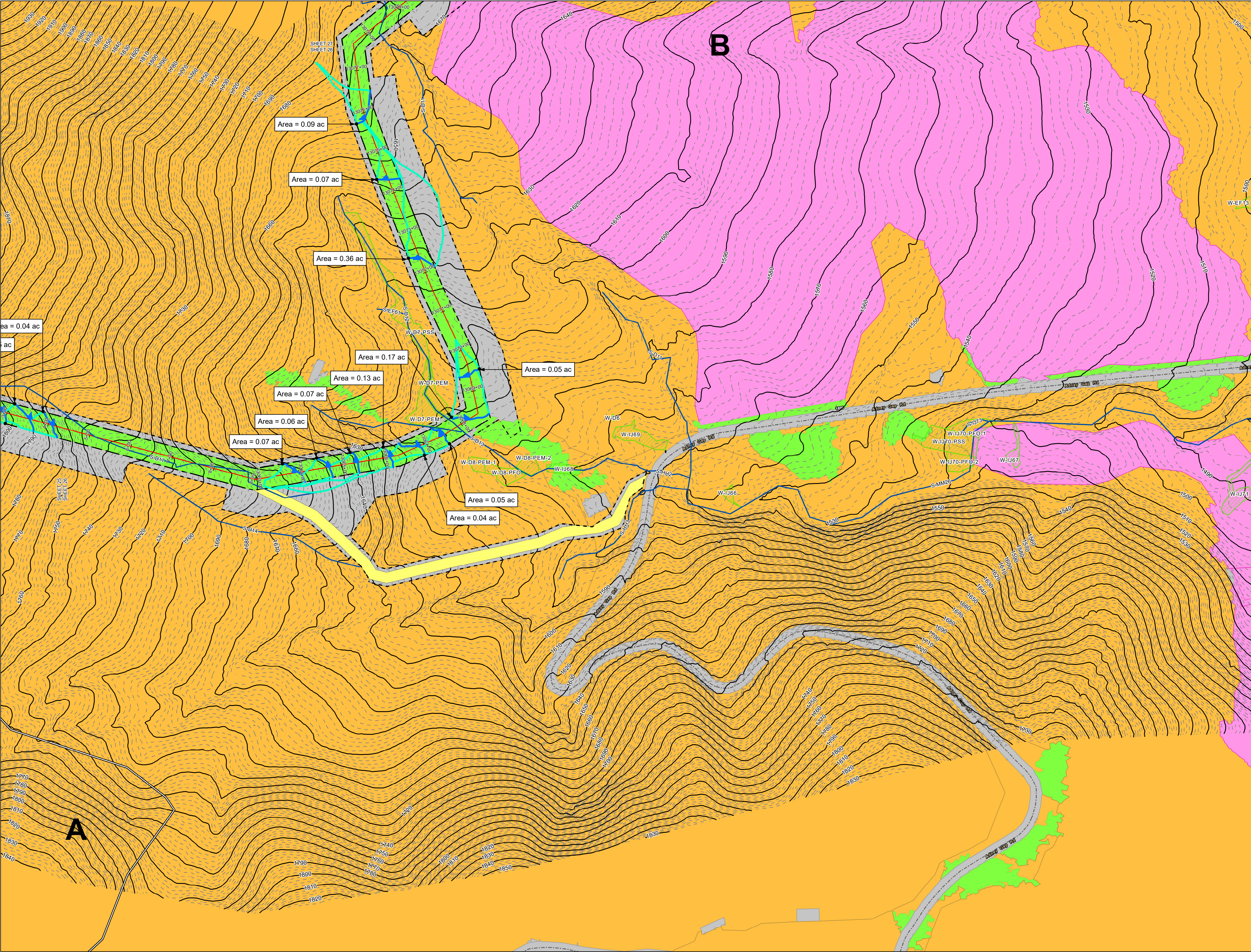
Mountain Valley Pipeline Project



**Clean Water Diversion Pipe
Drainage Area Map
Spread 10**

Figure 6 of 11
Franklin County
August, 2018

Data Sources: ESRI Streaming Data 2014.



Legend

	Karst Feature		Water Bar
	Approximate Location of Water Bar End Treatment		100-year Floodplain
	Permanent Water Bar 10-ft End Treatment		Pond
	Permanent Water Bar 15-ft End Treatment		Wetland
	Permanent Water Bar 20-ft End Treatment		Hydrologic Soil Groups
	Sheetflow		100 ft Buffer off of Limits of Disturbance
	Shallow Concentrated Flow		Agricultural
	Streams		Barren
	Alignment Centerline		Brush
	Permanent Easement		Forest
	MLV Site		Impervious
	Access Road Permanent Easement		Meadow
	Existing Impervious Surveyed Road Edge		Open Water
	New/Proposed Impervious Road Edge		10-foot Contour
			2-foot Contour
			State Road Centerline
			Railroad

Notes:

1) Note that only waterbars with a number designation required site specific analysis. Refer to "Appendix - Spread 10 Site Specific Analyses" for all calculations related to waterbar and treatment and drainage area analysis.

2) Unless otherwise noted, the water bar drainage areas on this sheet are less than or equal to 1.5-acres and have a CN less than or equal to 71 and thus do not need a site specific calculation. In HSG A and B soils, it can be determined by inspection if the CN exceeds 71 because impervious cover must exceed 60% in A soils and 32% in B soils (assuming a worst case of meadow conditions in the remainder of the water bar drainage area). A weighted CN is provided for water bar drainage areas with HSG C soils and any impervious cover. Water bar drainage areas with HSG D soils are assumed to have a CN greater than 71. A site specific calculation is provided if the water bar drainage area is greater than 1.5-acres or has a CN greater than 71. Site specific calculations will use the Rational Method equation with runoff coefficients contained in VASWMH Table 4-5a and 4-5b.

3) Per the Approved Test Area Stormwater Narrative (1/22/2018), Section II.A and II.B, the 75-foot temporary construction and 50-foot permanent ROW will be restored to predevelopment conditions except where that condition is forested. In this case the 75-foot temporary construction LOD post-development condition will be brush (seeded with a mix of herbaceous and woody species) and may naturally return to forest condition subject to landowner actions; and the 50-foot permanent ROW when indicated will be seeded and restored to meadow conditions.

NAD 1983 UTM 17N

1" = 100 feet

100 0 100 Feet

Mountain Valley Pipeline Project

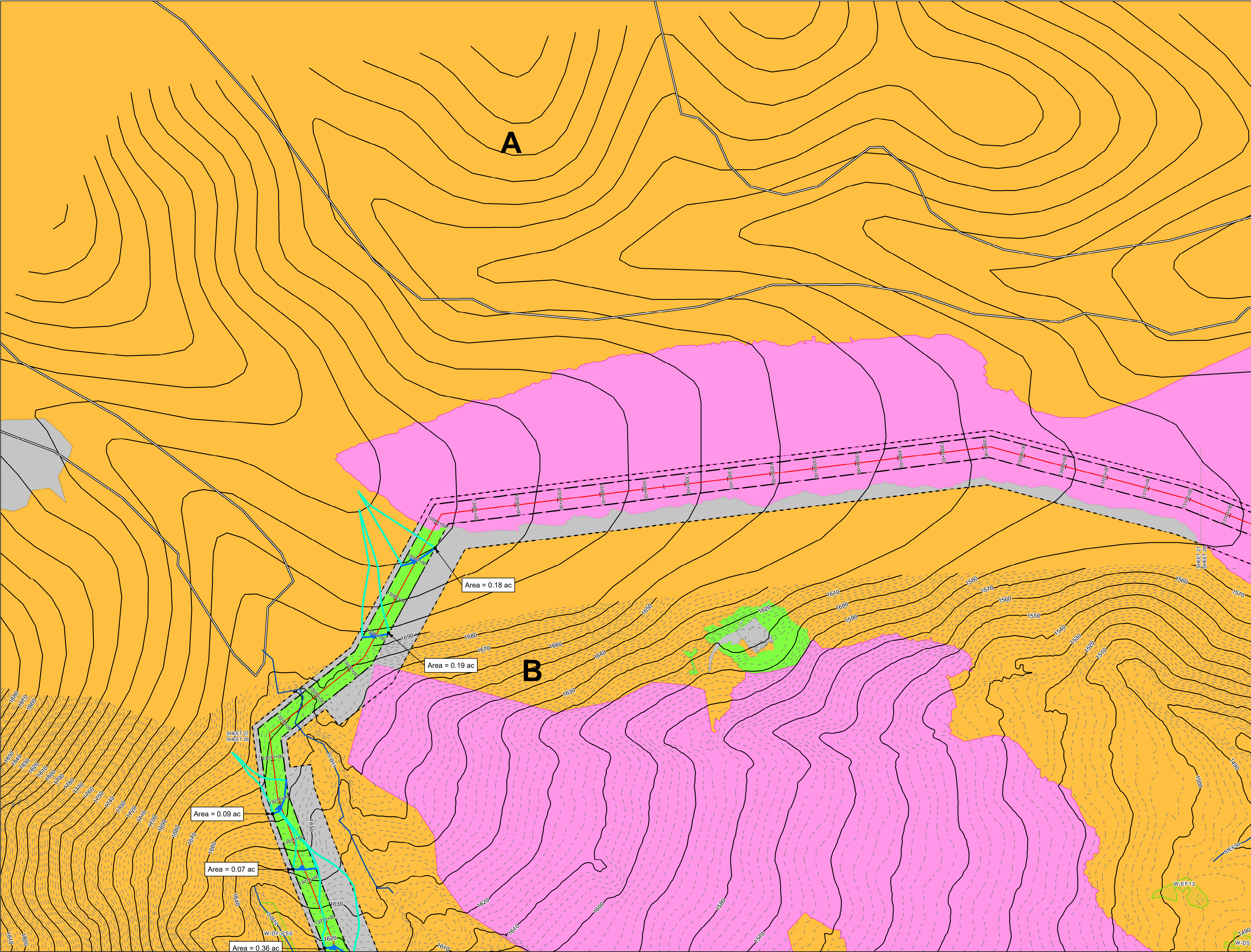
Drainage Map Spread 10

Figure 26 of 55
Franklin County
August, 2018

Pipeline Stationing -	From 13053+00-5+00	To 13079+00
Post Construction Plan No.	14.28PC	14.29PC

Data Sources: Imagery from ESRI Streaming Data 2014, Delineated streams surveyed by Tetra Tech Inc. 2014 to 2017, Elevation data derived from LIDAR provided by EQT 2016, Soils from NRCS Gridded Soil Survey Geographic (SSURGO) database 2014, Forest cover land use from the VGIN Land Cover Dataset, Transportation data from VITA map layer 2016, Existing and proposed roads were surveyed by EQT.

Document Path: PGH P:\GIS\EQT_MVP\Mapdocs\Drainage\MXD\MVP_Drainages_Spread10_36x24.mxd



Legend

	Karst Feature		Water Bar Drainage Area
	Approximate Location of Water Bar End Treatment		100-year Floodplain
	Permanent Water Bar 10-ft End Treatment		Pond
	Permanent Water Bar 15-ft End Treatment		Wetland
	Permanent Water Bar 20-ft End Treatment		Hydrologic Soil Groups
	Sheetflow		100 ft Buffer off of Limits of Disturbance
	Shallow Concentrated Flow		Agricultural
	Streams		Barren
	Alignment Centerline		Brush
	Permanent Easement		Forest
	MLV Site		Impervious
	Access Road Permanent Easement		Meadow
	Existing Impervious Surveyed Road Edge		Open Water
	New/Proposed Impervious Road Edge		10-foot Contour
			2-foot Contour
			State Road Centerline
			Railroad

Notes:

1) Note that only waterbars with a number designation required site specific analysis. Refer to "Appendix - Spread 10 Site Specific Analyses" for all calculations related to waterbar end treatment and drainage area analysis.

2) Unless otherwise noted, the water bar drainage areas on this sheet are less than or equal to 1.5-acres and have a CN less than or equal to 71 and thus do not need a site specific calculation. In HSG A and B soils, it can be determined by inspection if the CN exceeds 71 because impervious cover must exceed 60% in A soils and 32% in B soils (assuming a worst case of meadow conditions in the remainder of the water bar drainage area). A weighted CN is provided for water bar drainage areas with HSG C soils and any impervious cover. Water bar drainage areas with HSG D soils are assumed to have a CN greater than 71. A site specific calculation is provided if the water bar drainage area is greater than 1.5-acres or has a CN greater than 71. Site specific calculations will use the Rational Method equation with runoff coefficients contained in VASWMH Table 4-5a and 4-5b.

3) Per the Approved Test Area Stormwater Narrative (1/22/2018), Section II.A and II.B, the 75-foot temporary construction and 50-foot permanent ROW will be restored to predevelopment conditions except where that condition is forested. In this case the 75-foot temporary construction LOD post-development condition will be brush (seeded with a mix of herbaceous and woody species) and may naturally return to forest condition subject to landowner actions; and the 50-foot permanent ROW when indicated will be seeded and restored to meadow conditions.

NAD 1983 UTM 17N

1" = 100 feet

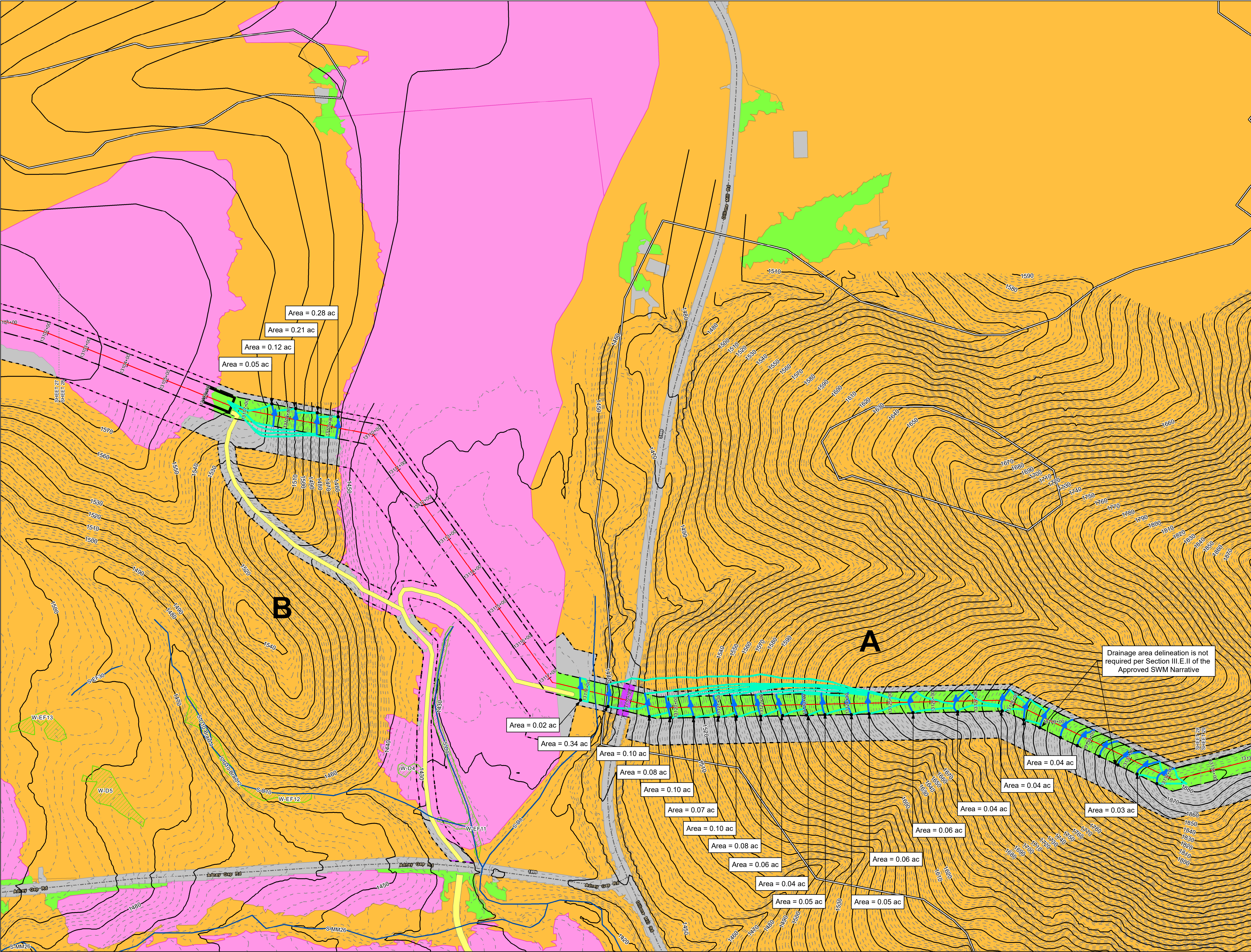
100 0 100 Feet

Mountain Valley Pipeline Project

Drainage Map
Spread 10
Figure 27 of 55
Franklin County
August, 2018

Pipeline Stationing -	From 13073+00	To 13102+00
Post Construction Plan No.	14.28PC	14.29PC

Data Sources: Imagery from ESRI Streaming Data 2014. Delineated streams surveyed by Tetra Tech Inc. 2014 to 2017. Elevation data derived from LIDAR provided by EQT 2016. Soils from NRCS Gridded Soil Survey Geographic (SSURGO) database 2014. Forest cover land use from the VGIN Land Cover Dataset. Transportation data from VITA map layer 2016. Existing and proposed roads were surveyed by EQT.



Legend

	Karst Feature		Water Bar Drainage Area
	Approximate Location of Water Bar End Treatment		100-year Floodplain
	Permanent Water Bar 10-ft End Treatment		Pond
	Permanent Water Bar 15-ft End Treatment		Wetland
	Permanent Water Bar 20-ft End Treatment		Hydrologic Soil Groups
	Sheetflow		100 ft Buffer off of Limits of Disturbance
	Shallow Concentrated Flow		Agricultural
	Streams		Barren
	Alignment Centerline		Brush
	Permanent Easement		Forest
	MLV Site		Impervious
	Access Road Permanent Easement		Meadow
	Existing Impervious Surveyed Road Edge		Open Water
	New/Proposed Impervious Road Edge		10-foot Contour
			2-foot Contour
			State Road Centerline
			Railroad

Notes:

1) Note that only waterbars with a number designation required site specific analysis. Refer to "Appendix - Spread 10 Site Specific Analyses" for all calculations related to waterbar and treatment and drainage area analysis.

2) Unless otherwise noted, the water bar drainage areas on this sheet are less than or equal to 1.5-acres and have a CN less than or equal to 71 and thus do not need a site specific calculation. In HSG A and B soils, it can be determined by inspection if the CN exceeds 71 because impervious cover must exceed 60% in A soils and 32% in B soils (assuming a worst case of meadow conditions in the remainder of the water bar drainage area). A weighted CN is provided for water bar drainage areas with HSG C soils and any impervious cover. Water bar drainage areas with HSG D soils are assumed to have a CN greater than 71. A site specific calculation is provided if the water bar drainage area is greater than 1.5-acres or has a CN greater than 71. Site specific calculations will use the Rational Method equation with runoff coefficients contained in VASWMH Table 4-5a and 4-5b.

3) Per the Approved Test Area Stormwater Narrative (1/22/2018), Section II.A and II.B, the 75-foot temporary construction and 50-foot permanent ROW will be restored to predevelopment conditions except where that condition is forested. In this case the 75-foot temporary construction LOD post-development condition will be brush (seeded with a mix of herbaceous and woody species) and may naturally return to forest condition subject to landowner actions; and the 50-foot permanent ROW when indicated will be seeded and restored to meadow conditions.

NAD 1983 UTM 17N

1" = 100 feet

100 0 100 Feet

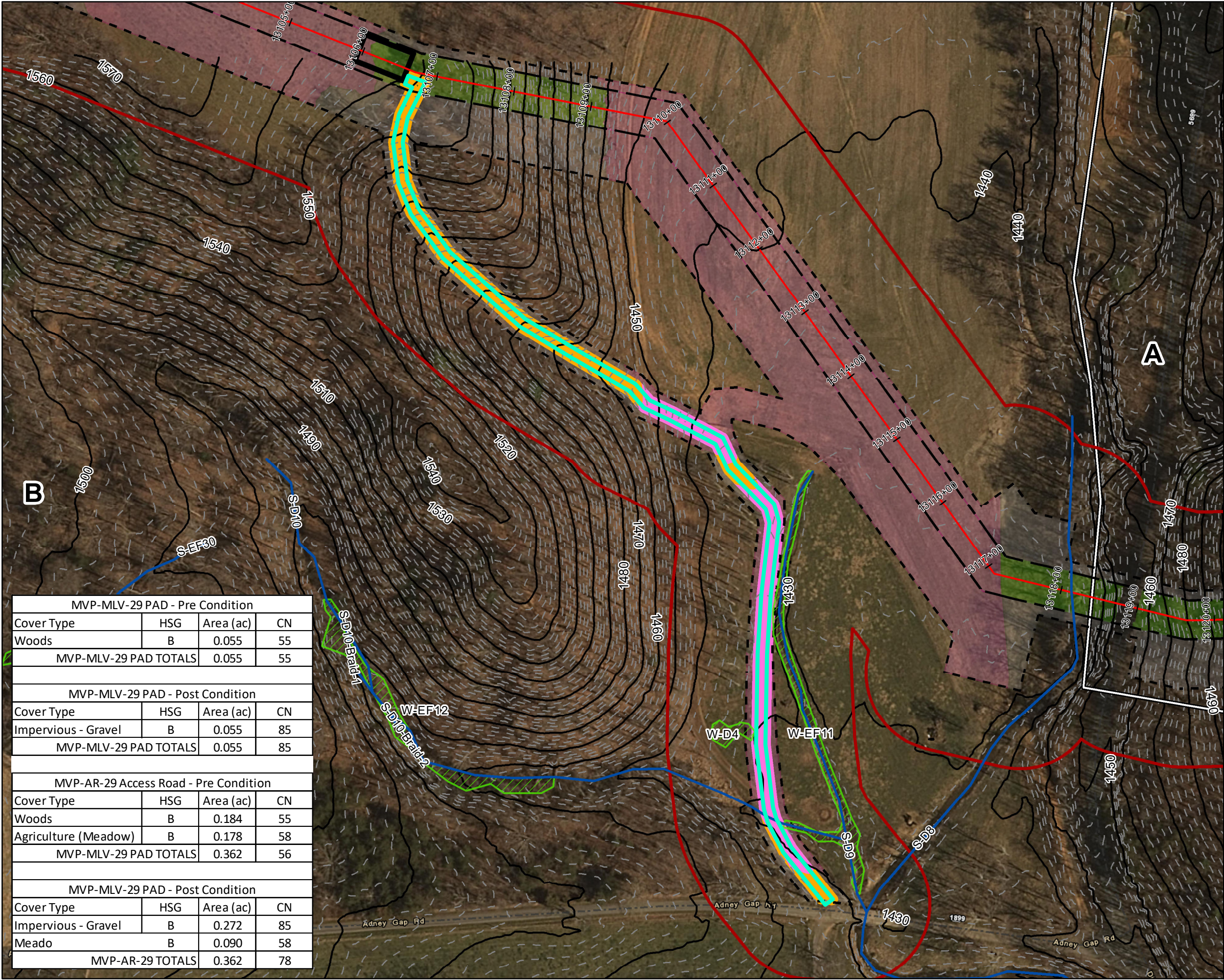
Mountain Valley Pipeline Project

Drainage Map Spread 10

Figure 28 of 55
Franklin County
August, 2018

Pipeline Stationing -	From 13102+00	To 13133+00
Post Construction Plan No.	14.29PC	14.31PC

Data Sources: Imagery from ESRI Streaming Data 2014, Delineated streams surveyed by Tetra Tech Inc. 2014 to 2017. Elevation data derived from LIDAR provided by EQT 2016, Soils from NRCS Gridded Soil Survey Geographic (SSURGO) database 2014, Forest cover land use from the VGIN Land Cover Dataset, Transportation data from VITA map layer 2016, Existing and proposed roads were surveyed by EQT.



MVP-MLV-29 PAD - Pre Condition			
Cover Type	HSG	Area (ac)	CN
Woods	B	0.055	55
MVP-MLV-29 PAD TOTALS		0.055	55
MVP-MLV-29 PAD - Post Condition			
Cover Type	HSG	Area (ac)	CN
Impervious - Gravel	B	0.055	85
MVP-MLV-29 PAD TOTALS		0.055	85
MVP-AR-29 Access Road - Pre Condition			
Cover Type	HSG	Area (ac)	CN
Woods	B	0.184	55
Agriculture (Meadow)	B	0.178	58
MVP-MLV-29 PAD TOTALS		0.362	56
MVP-MLV-29 PAD - Post Condition			
Cover Type	HSG	Area (ac)	CN
Impervious - Gravel	B	0.272	85
Meado	B	0.090	58
MVP-AR-29 TOTALS		0.362	78

Legend

Streams

Stationing

Alignment Centerline

Permanent Easement

Limit of Disturbance

MLV Pad

New Access Road

Access Road Drainage Area

100-year Floodplain

Pond

Wetland

Hydrologic Soil Groups

100 ft Buffer off of Limits of Disturbance

Agricultural

Barren

Brush

Meadow

Agricultural

Forest

Existing Impervious

Meadow

State Road Centerline

10-foot Contour

2-foot Contour

NAD 1983 UTM 17N (feet)

1 in = 120 feet

120

60

0

120

Feet

N

W

E

S

Mountain Valley Pipeline Project

New Impervious Cover Stormwater Drainage Exhibits

MLV-29 Spread 10

Figure 007
Franklin County, Virginia
September 2018

Data Sources: Imagery from ESRI Streaming Data 2014, Delineated streams surveyed by Tetra Tech Inc. 2014 to 2017, Transportation data from VITA map layer 2016, Elevation data derived from LIDAR provided by EQT 2016, Soils from NRCS Gridded Soil Survey Geographic (SSURGO) database 2014, Land Use digitized from ESRI World Imagery 2015, Agricultural Area from National Land Cover Dataset 2011.

Document Path: P:\GIS\EQ\MVP\MapDocs\Drainage\MXD\MVP_Stormwater\Drainage_Exhibit_AccessRoad.mxd

i. New Impervious Cover: Access Roads

New impervious cover in Spread 10 includes three (3) access roads (MVP-MLV-AR-28 through -30). Increased volumes of stormwater runoff resulting from access roads will be controlled utilizing the methodology established in *MVP-33.1 through MVP-33.3 Gap Graded Gravel Detail for Mainline Valve Pads and Permanent Access Roads*.

Each access road consists of a geogrid, underlain by a 2-inch layer of clean-washed choker stone, geotextile fabric, an open-graded subbase reservoir, and compacted earthen baffles to detain water within the access road. The access road surface will consist of two gravel tracks, with a center aisle top-dressed with soil and seeded with a meadow seed mix per *MVP-ES11.2 Upland Meadow Seed Mix and Application Rates* or *MVP-ES11.3 Upland Steep Slope Seed Mix and Application Rates*.

Pre- and post-construction runoff volumes for the 10-year 24-hour storm were calculated using the Montgomery and Franklin County design storm values of 5.00 and 5.70 inches, respectively, per *PSS&S Section 4.2.2 Design Storms*. Runoff volumes were calculated for both the drainage area to each gap graded gravel access road and for the access road footprint alone. Results are shown below.

10-YEAR STORM DATA FULL RUN-ON DRAINAGE AREA					
SITE	TIME OF CONCENTRATION (PRE / POST) [HR]	CURVE NUMBER (PRE / POST)	DRAINAGE AREA [FT ²]	Q ₁₀ PEAK FLOW (PRE / POST) [CFS]	Q ₁₀ VOLUME (PRE / POST) [FT ³]
MLV-AR-28	0.16 / 0.16	71 / 71	456,413	30.45 / 30.39	80,296 / 80,297
MLV-AR-29	0.50 / 0.50	56 / 56	2,415,652	58.37 / 58.37	283,396 / 283,396
MLV-AR-30	0.13 / 0.13	82 / 82	43,339	5.31 / 5.31	13,387 / 13,387

10-YEAR STORM DATA ACCESS ROAD FOOTPRINT					
SITE	TIME OF CONCENTRATION (PRE / POST) [HR]	CURVE NUMBER (PRE / POST)	DRAINAGE AREA [FT ²]	Q ₁₀ PEAK FLOW (PRE / POST) [CFS]	Q ₁₀ VOLUME (PRE / POST) [FT ³]
MLV-AR-28	0.10 / 0.10	75 / 83	23,522	2.01 / 2.59	4,794 / 6,214
MLV-AR-29	0.10 / 0.10	56 / 78	15,784	0.72 / 1.83	1,865 / 4,351
MLV-AR-30	0.10 / 0.10	58 / 78	871	0.07 / 0.16	174 / 385

Increases in run-off volumes for both the drainage area and access road only are further summarized below.

		Peak Flow (cfs)	Hydrograph Volume (ac-ft)	Hydrograph Volume (ft ³)	Required Treatment Volume (ft ³)
MLV-AR-28 FULL DA	Pre	30.45	1.84334	80296	1
	Post	30.39	1.84337	80297	
MLV-AR-28 AR ONLY	Pre	2.01	0.11006	4794	1420
	Post	2.59	0.14265	6214	

MLV-AR-29 FULL DA	Pre	58.37	6.50588	283,396	0
	Post	58.37	6.50588	283,396	
MLV-AR-29 AR ONLY	Pre	0.72	0.04281	1,865	2,486
	Post	1.83	0.09989	4,351	

MLV-AR-30 FULL DA	Pre	5.31	0.30732	13387	0
	Post	5.31	0.30732	13387	
MLV-AR-30 AR ONLY	Pre	0.04	0.00262	114	126
	Post	0.1	0.00551	240	

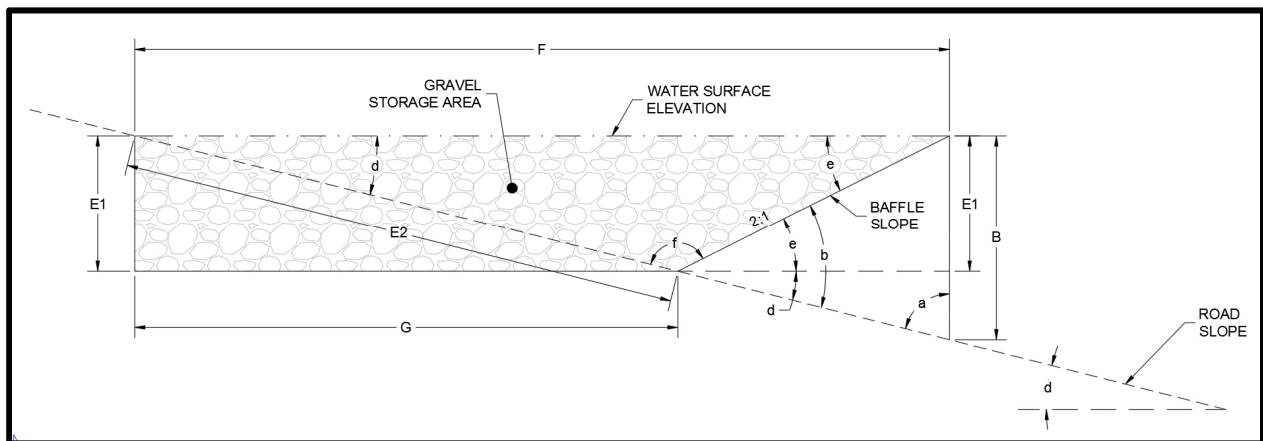
The runoff volume increase when considering only the access road is greater than the resulting runoff volume increase when considering the full drainage area. As a result, the reservoir within the access road is conservatively sized to accommodate the required volume computed using the road footprint only. Any increase in runoff volume from pre- to post-construction condition must be stored within the gap graded gravel to meet flood protection requirements per 9VAC25-870-66.C.2.

A site-specific analysis was performed for all access roads to determine the number of earthen baffles, earthen baffle spacing and subbase reservoir depth required to detain the increased volume from the 10-year storm, and allow the excess stormwater to infiltrate into the underlying soil. Details of the analysis are provided below.

Site	Road Length (ft)	Road Slope (ft/ft)	# of Baffles	Baffle Spacing (ft)	Baffle Height (ft)
MVP-MLV-AR-28	190	0.110	4	47	1
	170	0.142	2	85	1
	90	0.225	1	90	1
	92	0.087	2	46	1
	80	0.022	1	80	1
	106	0.082	4	26	1
	244	0.118	2	122	1
	141	0.050	2	70	1

	158	0.042	2	79	1
	100	0.115	4	25	1
	150	0.048	2	75	1
	293	0.291	4	73	1
	69	0.202	3	23	1
	28	0.067	1	28	1
MVP-MLV-AR-29	400	0.002	1	400	1
	270	0.026	1	270	1
	320	0.158	1	320	1
	257	0.211	1	257	1
	65	0.086	1	65	1
MVP-MLV-AR-30	70	0.001	1	70	.05

Because the slopes of the access roads vary significantly, storage calculations were performed for each, using the following methodology:



1. Determine the cross-section area (CSA) of storage behind each baffle, assuming a triangle based on bottom slope.

$$CSA = 0.5 \times A \times F \times \sin(e) + 0.5 \times E1 \times E2 \times \sin(a)$$

where CSA = Cross-sectional area; ft²

$$a = 90 - \tan^{-1}(\text{road slope})$$

$$A = B \times (\sin(a)/\sin(b))$$

$$b = \tan^{-1}(\text{road slope}) + \tan^{-1}(\text{baffle slope})$$

$$B = \text{baffle height}$$

$$d = \tan^{-1}(\text{road slope})$$

$$E1 = A \times \sin(e)$$

$$e = \tan^{-1}(\text{baffle slope})$$

$$E2 = A \times (\sin(e)/\sin(d))$$

$$f = 180 - b$$

$$F = A \times (\sin(f)/\sin(d))$$

$$G = F - E1/\text{baffle slope}$$

2. Determine the storage volume available per earthen baffle.

$$V_{\text{available}} = \text{CSA} \times W \times n$$

where $V_{\text{available}}$ = Storage volume per earthen baffle; ft³
 W = Stone width (12 ft)
 n = Stone porosity (0.40)

3. Determine the number of baffle cells needed by dividing the storage volume per earthen baffle into the required treatment volume. Because it is necessary to round up to the next integer, the baffle design volume will always exceed the required treatment volume.
4. Determine the baffle cell spacing by dividing the number of baffles needed into the access road length.

To ensure the roads drain with the 72-hour maximum drawdown time, the design volumes were divided by the most conservative saturated hydraulic conductivity (K_{sat}) of the underlying soils. Each calculated drawdown time used the maximum depth of each triangular CSA and was multiplied by a Safety Factor of 2, resulting in the following drawdown times (all less than the 72-hour maximum). Note that several access roads span more than one different soil types with different K_{sat} rates.

MVP-MLV-AR-28		
MUSYM	3E	[-]
HSG	B	[-]
K_{SAT}	1.46	[IN/HR]
Max Depth	0.96	[FT]
Drawdown Time	16	[HR]
MUSYM	29	[-]
HSG	D	[-]
K_{SAT}^{**}	0.26	[IN/HR]
Max Depth	0.92	[FT]
Drawdown Time*	43	[HR]
MUSYM	29	[-]
HSG	D	[-]
K_{SAT}^{**}	0.26	[IN/HR]
Max Depth	0.92	[FT]
Drawdown Time	43	[HR]

MVP-MLV-AR-29		
MUSYM	11A	[-]
HSG	B	[-]

K _{SAT}	1.30	[IN/HR]
Max. Depth	1.00	[FT]
Drawdown Time	18.4	[HR]
MUSYM	16E	[-]
HSG	B	[-]
K _{SAT}	1.98	[IN/HR]
Max. Depth	1.00	[FT]
Drawdown Time	11.0	[HR]
MUSYM	20E	[-]
HSG	B	[-]
K _{SAT}	1.99	[IN/HR]
Max. Depth	1.00	[FT]
Drawdown Time	7.2	[HR]
MUSYM	39C	[-]
HSG	B	[-]
K _{SAT}	1.50	[IN/HR]
Max. Depth	1.00	[FT]
Drawdown Time	8.5	[HR]

MVP-MLV-AR-30		
MUSYM	11A	[-]
HSG	B	[-]
K _{SAT}	1.3	[IN/HR]
Max Depth	0.50	[FT]
Drawdown Time	9	[HR]

*Note: 72-hour maximum drawdown time satisfied by reducing safety factor.

**Note: MUSYM 29 K_{SAT} assumed to equal MUSYM 25 K_{SAT}.

ii. New Impervious Cover: Main Line Valve Pads

New impervious cover in Spread 11 also includes five (5) main line valve sites (MVP-MLV-31 through -35). Increased volumes of stormwater runoff resulting from the main line valve pads will be controlled utilizing the methodology established in *MVP-33.1 through MVP-33.3 Gap Graded Gravel Detail for Mainline Valve Pads and Permanent Access Roads*. All pads will be located on relatively flat ground. The runoff volume increase when considering only the pad is greater than the resulting runoff volume increase when considering the full drainage area. As a result, the reservoir within the gap graded gravel pad is conservatively sized to accommodate the required volume computed using the pad footprint only.

Pre- and post-construction runoff volumes for the 10-year 24-hour storm were calculated using the Montgomery and Franklin County design storm values of 5.00 and 5.70 inches, respectively, per *PSS&S Section 4.2.2 Design Storms*.

10-YEAR STORM DATA					
SITE	TIME OF CONCENTRATION (PRE / POST) [HR]	CURVE NUMBER (PRE / POST)	DRAINAGE AREA [FT ²]	Q ₁₀ PEAK FLOW (PRE / POST) [CFS]	Q ₁₀ VOLUME (PRE / POST) [FT ³]
MLV-28	0.10 / 0.10	55 / 85	2,396	0.07 / 0.28	174 / 653
MLV-29	0.10 / 0.10	55 / 85	2,376	0.10 / 0.26	269 / 617
MLV-30	0.10 / 0.10	58 / 85	2,396	0.12 / 0.33	305 / 784

Any increase in runoff volume from pre- to post-construction condition must be stored within the gap graded gravel to meet flood protection requirements per 9VAC25-870-66.C.2. The calculated treatment volume required was then divided by the pad footprint and 40% void space to determine the depth of gravel required to store the 10-year 24-hour storm event. In this instance, calculated gravel depths for all pads were less than the 8-inch minimum required per *MVP-33.1 through MVP-33.3 Gap Graded Gravel Detail for Mainline Valve Pads and Permanent Access Roads*. Therefore, gravel depths for all pads are 8 inches, providing storage beyond the 10-year 24-hour storm event.

MLV-28 Pad	Vreq	479	cf
	Area	2376	sf
	Dreq	0.50	ft
	Ddesign	8	in
	Vdesign	634	cf

MLV-29 Pad	Vreq	348	cf
	Area	2376	sf
	Dreq	0.37	ft
	Ddesign	8	in
	Vdesign	634	cf

MLV-30 Pad	Vreq	479	cf
	Area	2376	sf
	Dreq	0.50	ft

	Ddesign	8	in
	Vdesign	634	cf

To ensure the gravel pads drain with the 72-hour maximum drawdown time, the design volumes were divided by the most conservative saturated hydraulic conductivity (K_{sat}) of the underlying soils. Each calculated drawdown time was multiplied by a Safety Factor of 2, resulting in the following drawdown times, all less than the 72-hour maximum.

MVP-MLV-28		
MUSYM	3E	[-]
HSG	B	[-]
K_{SAT}	1.46	[IN/HR]
Depth	8	[IN]
Drawdown Time	11	[HR]

MVP-MLV-29		
MUSYM	39C	[-]
HSG	B	[-]
K_{SAT}	1.50	[IN/HR]
Depth	8	[IN]
Drawdown Time	10.7	[HR]

MVP-MLV-30		
MUSYM	11A	[-]
HSG	B	[-]
K_{SAT}	1.3	[IN/HR]
Depth	8	[IN]
Drawdown Time	12	[HR]

Results show the 10-year 24-hour storm event will be stored within the gravel layer with no overtopping, and with reasonable drawdown times before the next storm event.